## Ocean rogue waves and the NLS equation

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### **Christian Kharif**

Institut de Recherche sur les Phénomènes Hors Equilibre (IRPHE)

Ecole Centrale Marseille

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## **Observation of huge waves**

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Photo of a huge wave event

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### Photo of a huge wave event

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## Photo of a huge wave event

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Super tanker collisions with freak waves (1968-1994).

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#### Rogue waves in 2005 (Didenkulova et al, 2006)



Fig. 1. Events selected as true freak waves are marked by red stars (1 – ,Explorer", 2 – "Grand Voyager", 3 – "Norwegian Dawn", 4 – Kalk Bay, 5 – Blue Bay, 6 – Maracas Beach, 7 – Blake de Pastino, 8 – Port Orford, 9 – Petit Havre); yellow circles mark all other reported cases when abnormally large waves were observed.

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Figure 2. Freak wave A recorded on the 24th November, 1981 at the Gorm Field in the Danish Sector of the North Sea.



Figure 3. Freak wave B recorded on the 17th November, 1984 at the Gorm Field in the Danish Sector of the North Sea.



Figure 4. Freak wave C recorded on the 27th November, 1984 at the Gorm Field in the Danish Sector of the North Sea.

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#### Ferry collisions with rogue waves near the French coast

- ► The Pont Aven (L = 597 ft) hit a rogue wave (≈ 15 m) during the night 21-22 May 2006.
- ► The Louis Majesty (L = 207 m) hit a rogue wave (≈ 17 m) on 3 March 2010 and two passengers were killed.
- ► The Jean Nicoli (L = 200 m) hit a rogue wave ((≈ 20 m) on 6 March 2017.

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# Physical mechanisms of rogue wave generation

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- Wave-current interactions
- Geometrical or spatial focusing
- spatio-temporal focusing or dispersive focusing
- modulational instability (resonant four-wave interaction)
- crossing seas
- soliton collision
- etc.

• Mathematically, a rogue wave of height  $H_f$  satisfies

 $H_f > 2H_s$ 

- ► H<sub>f</sub> is more than twice the significant height H<sub>s</sub> or 8 times the rms of the surface elevation
- Waves with larger heights than expected based on the Rayleigh distribution (abnormal waves)
- The above definition was proposed by Soren Peter Kjelsen in 1989 during the Workshop on Water Wave Kinematics, Molde (Norway)
- Water Wave Kinematics, Nato ASI series, eds. A.Torum & O.T. Gudmestad, 1990



Cumulative distribution function (%) as a function of normalized wave height  $H/H_s$  (from Sand *et al*, 1989) corresponding to North Sea data during stormy weather

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# Modulated water waves without and with the presence of a shear current

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#### Wind waves in the Large Air-Sea Interaction Facility (LASIF)



Fetch: 18 *m* and wind speed:  $10 m \cdot s^{-1}$  from (H. Branger)

#### Wind waves in open field



Fetch: 80 km and wind speed:  $7 m \cdot s^{-1}$  (from H. Branger)

 This strong group structure of the wave field or modulational aspect of the surface elevation is due to resonant 4-wave interactions

An elegant analytical method to study nonlinear modulational processes is the nonlinear Schrödinger equation

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# The nonlinear Schrödinger equation (NLS equation)

- governs the spatio-temporal evolution of the complex envelope of the free surface of weakly nonlinear and dispersive water waves
- is a universal equation that can be derived from the nonlinear water wave equations using the method of multiple scales
- was first derived within the framework of water waves by Benney & Newell (1967)

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Let us consider a weakly nonlinear modulated wave train propagating on finite depth at the free surface of a shear current of constant vorticity

$$\eta(x,t) = \frac{1}{2} (\epsilon a(\xi,\tau) \exp[i(kx - \omega t)] + c.c) + \mathcal{O}(\epsilon^2)$$
  
where  $\xi = \epsilon(x - c_g t)$  and  $\tau = \epsilon^2 t$ .

Starting from the nonlinear water wave equations and using the method of multiple scales, the evolution of the complex envelope is governed by the NLS equation

$$i(a_{ au}+c_{g}a_{\xi})+La_{\xi\xi}+N\mid a\mid^{2}a=0$$

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$$L = \frac{\omega}{k^2 \sigma (2+X)} \{ \mu (1 - \sigma^2) [1 - \mu \sigma + (1 - r)X] - \sigma r^2 \}$$

$$N = -\frac{\omega k^2 (U + VW)}{2(1 + X)(2 + X)\sigma^4}$$

$$U = 9 - 12\sigma^2 + 13\sigma^4 - 2\sigma^6 + (27 - 18\sigma^2 + 15\sigma^4)X$$

$$+ (33 - 3\sigma^2 + 4\sigma^4)X^2 + (21 + 5\sigma^2)X^3 + (7 + 2\sigma^2)X^4 + X^5$$

$$V = (1 + X)^2(1 + r + \mu\overline{\Omega}) + 1 + X - r\sigma^2 - \mu\sigma X$$

$$W = 2\sigma^3 \frac{(1 + X)(2 + X) + r(1 - \sigma^2)}{\sigma r(r + \mu\overline{\Omega}) - \mu(1 + X)}$$
ere  $\mu = kh, \sigma = tanh(\mu), r = c_g/c_p, \overline{\Omega} = \Omega/\omega(\Omega) \text{ and } X = \sigma\overline{\Omega}$ 

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In deep water without shear current the coefficients reads

$$L = -\frac{\omega}{8k^2}$$
 and  $N = -\frac{1}{2}\omega k^2$ 

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 The vor-NLS equation admits the following Stokes' wave solution

$$a = a_0 \exp(iNa_0^2\tau)$$

Perturbation

$$a = a_0(1 + \delta a) \exp[i(\delta \omega + Na_0^2 \tau)]$$

with

$$\delta a = (\delta a)_0 \exp[i(l\xi - \lambda \tau)]$$
$$\delta \omega = (\delta \omega)_0 \exp[i(l\xi - \lambda \tau)]$$

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 Condition of linear instability with respect to sideband perturbations

LN > 0

Let 
$$L = L_1 \omega / k^2$$
 and  $N = N_1 \omega k^2$ 

 Modulational instability occurs for perturbations whose wavenumber / satifies

$$-\sqrt{2\frac{N_1}{L_1}}ka_0 < \frac{l}{k} < \sqrt{2\frac{N_1}{L_1}}ka_0$$

- The growth rate of instability is  $\gamma = \frac{l\omega}{k^2} \sqrt{2N_1L_1k^4a_0^2 - l^2L_1^2}$
- Maximal growth rate

$$\gamma_{\max} = -N_1 \omega (a_0 k)^2$$
 for  $I_{\max} = \sqrt{N_1/L_1} a_0 k^2$ 

• For 
$$\Omega < -2\sqrt{\frac{gk}{3\sigma}} \Rightarrow$$
 no BF instability

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#### Nonlinear evolution of BF instability



Envelope of surface elevation of a Stokes wave train of initial steepness  $|A_0|k = 0.125$  amplified by its most unstable perturbation (FPU recurrence)

$$i\frac{\partial q}{\partial T} + \frac{\partial^2 q}{\partial X^2} + 2 |q|^2 q = 0$$
  
with  
$$T = \frac{1}{2}\omega\tau, \qquad X = 2k\xi, \qquad q = \frac{1}{\sqrt{2}}kA^*$$



#### Temporal evolution of the carrier mode and satellites

#### Experimental spectrum evolution of modulated waves



Carrier wave steepness 0.07 (without wind, from H. Branger)

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Application to Rogue Waves when modulational instability prevails

- The key parameter measuring the importance of the nonlinear four-wave interaction is the Benjamin-Feir Index (BFI) which is the ratio of the wave steepness to the normalized spectral bandwidth.
- Within the framework of the NLS equation the BFI writes

$$BFI = \frac{a_0 k}{\Delta K/k} \sqrt{\mid N_1/L_1 \mid}$$

where  $\Delta K$  is a typical spectral bandwidth (Onorato *et al*, 2006 and Kharif *et al*, 2009)

The BFI is a convenient indicator for prediction of rogue wave occurrence. It is related to the pdf of wave heights. The rogue wave probability occurrence increases with the BFI.



Normalized BFI as a function of *kh* for several values of  $\overline{\Omega}$ :  $\overline{\Omega} = 0$  (solid line),  $\overline{\Omega} = 1$  (dashed line),  $\overline{\Omega} = 2$  (dot-dashed line)

Thomas, Kharif & Manna (POF, 2012)



Normalized BFI as a function of *kh* for several values of  $\overline{\Omega}$ :  $\overline{\Omega} = 0$  (solid line),  $\overline{\Omega} = -0.3$  (dashed line),  $\overline{\Omega} = -0.6$  (dot-dashed line)

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#### ISBN 978-3-540-88418-



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AGEM<sup>2</sup> Print ISSN: 1866-8348 Online ISSN: 1866-835

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